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<p>(54) Title: CHEMICALLY MODIFIED SOLID PHASE EXTRACTION PARTICLES AND ARTICLES CONTAINING SAME</p> <p>(57) Abstract</p> <p>A functionalized macroporous poly(styrene divinylbenzene) particle comprises at least one ionic functional group covalently bonded thereto, the functionalized particle having sorptive capability towards an analyte, said functional group being present in the range of 0.1 to 2.5 milliequivalents per gram of poly(styrene divinylbenzene). The functionalized particles can be used in a packed column or enmeshed in a nonwoven web for utility in solid phase extraction applications.</p>		

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CHEMICALLY MODIFIED SOLID
PHASE EXTRACTION PARTICLES AND
ARTICLES CONTAINING SAME

FIELD OF THE INVENTION

10 This invention relates to particles useful for solid phase extraction (SPE) processes, which particles have been partially chemically modified under controlled conditions to optimize sorptive properties. In another aspect, there are disclosed methods of
15 making the particles and using the particles in packed columns and in composite sheet-like articles of the invention.

BACKGROUND OF THE INVENTION

20 Classical methods for separating analytes from water and other fluids use liquid/liquid extraction (LLE) procedures wherein the analyte is preferentially partitioned from an aqueous based liquid into an immiscible extraction liquid phase. Efficiency and
25 selectivity of extraction of specific analytes by LLE is dependent on the partition coefficient of the analyte between the two liquids and is limited by the type of extraction liquid that can be used. Recently, solid phase extraction (SPE) procedures have been
30 developed using solid particulate phases which can interact with the analyte by ion exchange, chelation, covalent bond formation, size exclusion, sorption, and other mechanisms to bind and remove the analyte from the fluid. SPE processes are described in Analytica
35 Chimica Acta, 236, 157-164 (1990) and LC/GC, 9:5, 332-337 (1991). Application of mixed-mode SPE using copolymerized mixed-mode resins where C₁₈ (octadecyl) and sulfonic acid functional groups are in closer

proximity than on "blended" mixed mode resins is reported in J. Chrom. 629 (1993) 11-21.

The type of SPE particulate chosen to effect separation of specific analytes can be inorganic, inorganic with organic coatings, inorganic with covalently bonded organic functional groups, polymeric organic resins and derivatives thereof.

U.S. Patent No. 4,895,662 describes a process for purification of aqueous effluent from bleaching of wood pulp using macroporous adsorbent resins having been post-crosslinked in the swollen state and functionalized with hydrophilic groups prior to contact with the waste effluent.

U.S. Patent Nos. 5,104,545 and 5,135,656 describe a process for removing water soluble metal salts of organic acids from oil field water using nonionogenic macroreticular adsorption resins such as XAD-16™ from Rohm and Haas Co., Philadelphia, PA.

U.S. Patent Nos. 5,071,565 and 5,230,806 describe neutral functionalized resins which take up organics by adsorption rather than ion exchange and teach that the amount of functional group relative to the amount of poly(styrene divinylbenzene) is not critical. They teach that the functional group must be neutral since anionic or cationic resins may pick up undesirable materials that are present. Utility of these resins for SPE of phenols was reported by J.S. Fritz et al. in J. Chrom. 641 (1993) 57-61.

U.S. Patent No. 5,114,591 describes ion exchange resins for reducing organic material content of paint booth waste water having functional groups that provide ion exchange activity and also adsorb neutral molecules in varying degrees.

U.S. Patent No. 5,236,594 describes a process for removing specific toxicants containing at least one

carboxylate group from aqueous petroleum waste streams using non-ionic macroreticular polymeric resins.

U.S. Patent No. 4,537,683 describes anion exchange particles alone or anion exchange particles combined with cation exchange particles in the form of a floc. It is reported that the level of ion exchange functionality has only a limited effect on the particles' ability to remove trihalomethane precursors.

U.S. Patent No. 5,279,742 describes solid phase extraction media and methods using sorptive particulate in particulate loaded PTFE matrix sheet configurations wherein disks of the same or different compositions can be stacked to achieve separations.

A major requirement for particulate useful for SPE is that it has sufficient sorptive capacity to retain the analyte of interest. The retention characteristics of a specific analyte by a sorptive particulate is expressed numerically as its "capacity factor (k')", see "Contemporary Practice of Chromatography", C. F. Poole and S. A. Schuette, Elsevier, New York, NY (1984) pp 2-6.

J. J. Sun and J. S. Fritz in J. Chrom. 522 (1990) 95-105 describe chemical modifications of polymeric resins to increase analyte capacity factor (k') for high performance liquid chromatography applications.

SUMMARY OF THE INVENTION

Briefly, the present invention provides a functionalized macroporous poly(styrene divinylbenzene) particle comprising ionic (cationic or anionic) functional groups covalently bonded thereto, the functionalized particle having sorptive capability towards an analyte, the functional group being present in a concentration range of 0.1 to 2.5 milliequivalents

per gram of functionalized poly(styrene divinybenzene).

Preferably, the functionalized particle exhibits a maximum range in retentive capacity for selected
5 analytes dependent on the level of functional (i.e., substituted) group present.

Preferably, the analyte exhibits a maximum value of capacity factor (k') using functionalized poly(styrene divinybenzene) particles in the specified
10 exchange concentration range compared to a lesser value of capacity factor (k') for the same analyte for similarly functionalized particles present in an amount outside the ion exchange concentration range.

Surprisingly, the maximum in retentive capacity is not
15 coincident with the maximum possible concentration of the functional group. The particles are useful in solid phase extraction applications, both when packed in columns and when incorporated in fibrous membranes.

In another aspect, the functionalized particles of
20 the invention comprising cationic or anionic functional groups in the ion exchange concentration range designated above, exhibit superior wetting properties towards liquids, preferably aqueous-based liquids, compared to functionalized particles comprising
25 functional groups outside the designated ion exchange concentration range. Aqueous-based liquids include water, optionally in combination with at least one of miscible organic liquids and inorganic species.

In a further aspect, the solid phase extraction
30 particles of the invention can be packed in a column or bed, or the particles can be incorporated into a porous fibrous membrane to provide a porous fibrous medium in sheet form, and one or a stack of such media can be useful in applications in separations science.

In yet another aspect, the present invention provides a method of optimizing sorptive properties wherein the capacity factor (k') of an analyte to be sorbed by functionalized poly(styrene divinylbenzene) particulate is maximized, the method comprising the step of providing a poly(styrene divinylbenzene) particle having covalently bonded thereto in the ion exchange concentration range of 0.1 to 2.5 milliequivalents of cationic or anionic functional groups per gram of functionalized polymer. The analyte exhibits a maximum in capacity factor (k') with respect to poly(styrene divinylbenzene) functionalized in the specified concentration range compared to (k') of the same analyte for similarly functionalized poly(styrene divinylbenzene) outside the designated concentration range.

In another aspect, the invention relates to a method of removing an analyte in a concentrated form from a solution by contacting the functionalized particle of the invention with the analyte for a time and at a temperature sufficient to bind the analyte to the particle. In a further step of the method, the invention relates to regenerating the functionalized particle by removing the analyte in a concentrated form from the functionalized particle, preferably by eluting the analyte with a suitable solvent.

Functionalized particles are prepared from macroporous poly(styrene divinylbenzene) particulates, which are commercially available (see, for example, U.S. Patent Nos. 4,501,826, 4,382,124, 4,297,220, 4,256,840, and 4,224,415), and the functionalization is achieved by methods known in the art.

It is believed to be novel in the art that controlled levels of chemical alteration (functionalization) of sorptive particulate can provide

optimum analyte retentive capacity and optimum wetting capability for particles used in solid phase extractions.

In this application:

5 "analyte" means the molecular species being isolated;

"capacity factor" (k') means a numerical measure of the retention characteristics of a specific analyte by a sorptive particulate (stationary phase). It is
10 defined as the ratio of the time spent by the analyte in the stationary phase to the time it spends in the mobile phase as expressed in Equation 1:

Equation 1: $k' = (t_r - t_m)/t_m$

15

where t_r is the analyte retention time in a column and t_m is the column dead time or the time of passage through the column of an unretained species; (k') varies with particle size, surface area, chemical
20 functionality of the sorbent particulate, and composition of the mobile phase;

"degree of derivatization", "ion exchange capacity", and "capacity" are used interchangeably;

"derivative of" or "derivatized" or

25 "functionalized" poly(styrene divinylbenzene) means poly(styrene divinylbenzene) having covalently bonded thereto at least one functional group which accepts protons or donates protons, which accepts electrons or donates electrons, or which shares electrons;

30 "hydrophilic" means having an affinity for, attracting, adsorbing, or absorbing water; preferably it means having a surface polarity of 0.5 or greater;

"hydrophobic" means lacking an affinity for, repelling, or failing to adsorb or absorb water;

preferably it means having a low surface polarity, for example, in the range of 0.1 to less than 0.5;

"macroporous resin", also known as "macroreticular resin", means a member of a class of highly crosslinked polymer particles penetrated by channels through which solutions can diffuse; often used as ion exchangers. Pores are regions between densely packed polymer chains. Pores less than 50 Angstrom are referred to as micropores, pores between 50 to 200 Angstroms are referred to as mesopores, and pores greater than 200 Angstrom are referred to as macropores;

"nonpolar compound" means molecules which have no permanent electric dipole moment;

"normal phase system" means a process using a more polar stationary phase with a less polar moving phase to effect separation of molecular species;

"particle" or "particulate" means a regular or irregular shaped particle, having an average size in the range of 0.1 to 150 micrometers, preferably in the range of 1 to 30 micrometers, and more preferably in the range of 5 to 20 micrometers; also included is polymeric fiber pulp having a length in the range of 0.8 mm to 4.0 mm and an average diameter in the range of less than 1 to 20 μm ;

"polar compound" means molecules which contain polar covalent bonds; they can ionize when dissolved; polar compounds include inorganic acids, bases, and salts;

"reversed phase system" means a process using a less polar stationary phase with a more polar moving phase to effect separation of molecular species;

"solid phase extraction" (SPE) means a process employing a solid phase for isolating classes of molecular species from fluid phases such as gases and liquids by sorption, ion exchange, chelation, size

exclusion (molecular filtration), affinity, ion pairing, etc. mechanisms;

"sorptive" or "sorption" or "sorbent" means capable of taking up and holding by either absorption
5 or adsorption;

"wettability" means the ability of any solid surface to be wetted when in contact with a liquid; that is, the surface tension of the liquid is reduced so that the liquid spreads over the surface; and

10 "wetting" means treatment of hydrophobic particulate or medium with an organic solvent, usually methanol, to provide higher polarity to the surface making it more accessible to high surface tension fluids such as water.

15 One problem encountered in the prior art is that hydrophobic sorptive particulate in packed columns or in particle loaded web composites used for SPE of hydrophobic analytes in water require a preliminary "wetting" step with solvents such as methanol. Wetting
20 is necessary because the low surface energy of the hydrophobic particles or composite does not allow high surface tension aqueous solutions efficient access to the high surface area of the sorptive particles' internal pores.

25 A number of approaches have been evaluated to increase the wettability or hydrophilicity of these particles and composites. One approach to eliminating or minimizing the wetting problem can be the addition of hydrophilic adjuvants such as micro-crystalline
30 cellulose fibers to composite sheet articles comprising polytetrafluoroethylene polymer (PTFE) or other hydrophobic fibrils and various sorptive particulate, as described in U.S. Patent No. 4,810,381. While this approach increases the overall hydrophilic character of
35 the composite, it does not address wetting of the

internal pores of entrapped sorptive particulate.
Intramolecular introduction of hydrophilic groups, for
example, on the macroporous poly(styrene
divinylbenzene) resin particles of the invention
5 provide "self wettability" of both external surfaces
and available internal pore surfaces.

No prior art of which we are aware discloses that
controlling the levels of ionic (cationic or anionic)
chemical modification of poly(styrene divinylbenzene)
10 taught by the instant invention can provide optimized
capacity factor (k') for separations. There is no
prior art evidence to suggest that specific
concentration levels of functionalization of
hydrophobic particles with hydrophilic groups will
15 provide optimum SPE properties especially with respect
to non-ionic neutral analytes. Indeed, intuition would
lead one of ordinary skill in the art to believe that
more functionalization is better. Surprisingly, the
present invention shows that improved separations are
20 realized at less-than-complete
functionalizations/concentrations. While it is
appreciated in the art that substitution of particles
with hydrophilic groups improves particle wettability,
it is an advance in the art to control the
25 concentration of the hydrophilic groups to provide
optimum wettability and analyte capacity factor (k').

BRIEF DESCRIPTION OF THE DRAWING

Fig. 1 is a series of four plots of phenol
30 capacity factor (k') vs. ion exchange capacity of
sulfonated poly(styrene divinylbenzene) resins.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS OF THE INVENTION

The functionalized particles of the invention can be prepared from poly(styrene divinylbenzene) particles. Particularly preferred particulate are:

5

	Material	Average Particle size	Trademark	Available from
10	highly cross-linked styrene and divinylbenzene copolymers, high performance material*	50-100 micrometers	Amberchrom™ CG-161m	Supelco, Inc. Bellefonte, PA
15	highly cross-linked styrene and divinylbenzene copolymer*	220-830 micrometers (ground to average size about 50 micrometers)	Amberlite™ XAD-2	Supelco, Inc. Bellefonte, PA
20	highly cross-linked styrene and divinylbenzene copolymer*	5-20 micrometers		Phenomenex, Inc., Torrance, CA Sarasep, Santa Clara, CA; Polymer Laboratories, Amherst, MA; Hamilton Co., Reno, NV

25

*Disclosed in one or more of U.S. Pat. Nos. 4,501,826, 4,382,124, 4,297,220, 4,256,840, 4,224,415

The functionalized poly(styrene divinylbenzene) particles can be cation or anion exchange particles. Strong cation exchangers include the particles functionalized by, for example, strong acid sulfonate (HSO₃) groups which are anionic; weak cation exchangers include the particles functionalized by, for example, carboxylate (COOH) groups which are anionic. Other functionalized poly(styrene divinylbenzene) particles can be strong anion exchangers which include the base particles functionalized by, for example, quaternary ammonium groups N⁺(R)₃ wherein each R independently can

be C_1 to C_4 alkyl groups. Weak anion exchangers include aminated groups $N(R^1)_2$ wherein each R^1 independently can be hydrogen, or C_1 to C_4 alkyl or alkanol groups.

Representative $N(R^1)_2$ groups include NH_2 , $N(C_2H_5)_2$,
5 $N(CH_3)_2$, and $N(C_2H_4OH)_2$, all of which are cationic.

In a preferred embodiment, the invention relates to poly(styrene divinylbenzene) particles which have been functionalized (i.e., chemically altered) by the addition of optimum levels of sulfonic acid groups to
10 at least one of ortho and para positions on the aromatic ring structure of the resin. Ring substitution by functional groups occurs in accordance with known rules of organic chemistry, see for example Carl. R. Noller, "Textbook of Organic Chemistry" W.B.
15 Saunders Company, Philadelphia, PA (1951) pp. 331-351. The functionalized particle can be prepared from the base particle which is mixed with glacial acetic acid and then reacted with concentrated sulfuric acid. The reaction can be quenched with water when the desired
20 degree of sulfonation is achieved. Details of this method are disclosed in Example 1, below.

It has been found that functionalization of the particles in the ion exchange concentration range of 0.1 to 2.5 milliequivalents of covalently bonded ionic
25 functionality per gram of functionalized polymer, preferably in the range of 0.15 to 2.0, more preferably in the range of 0.2 to 1.1 milliequivalents per gram, and most preferably in the ion exchange concentration range of 0.3 to less than 0.9 milliequivalents per gram
30 and even more preferred 0.3 to 0.8, and the very most preferred about 0.3 to 0.6 milliequivalents per gram provides maximum retentivity of polar or semi-polar analytes in solid phase extractions.

In one embodiment, the range of sulfonate chemical
35 modification levels to improve particle wettability

coincides with analyte capacity factor (k') enhancement to an optimum level of 0.6 milliequivalents per gram but further increased levels of sulfonate group substitution resulted in decreasing numerical values of the analyte capacity factor as shown in Figure 1. This range of functionalization also provides optimization of wetting characteristics of the particles. In SPE, the sulfonate functionalized particles can be effective in the absence of a wetting agent.

10 In a second embodiment, carboxylate functional poly(styrene divinylbenzene) can be prepared for use in solid phase extractions. In one method, poly(styrene divinylbenzene) resin particles can be chemically altered by oxidation of pendant groups such as aromatic
15 vinyl or aromatic alkyl groups to form carboxylate functional groups. Such oxidation can be performed as is known in the art, using, for example, oxidizing agents such as sodium hypochlorite, potassium permanganate, or dilute nitric acid, in amounts so as
20 to control the level of conversion to carboxylate groups. See, for example, Lee, Donald G., "The oxidation of organic compounds by permanganate ion and hexavalent chromium", Open Court Publishing Company: La Salle, IL, 1980, p. 43-64, and J. March, "Advanced
25 Organic Chemistry 3rd Ed.", Wiley-Interscience: New York, 1985. In a second method, varying levels of carboxylate functionality can be obtained by copolymerization of styrene, divinylbenzene, and a suitable carboxylic acid functional monomer such as
30 methacrylic acid. This second method has been described by R. Kunin in "Ion Exchange Resins", 2nd edition, Wiley: New York, (1958), p. 87, and by Meitzner et al., U.S. Patent No. 4,256,840.

The ability of organic resins to sorb certain
35 analyte molecules which are moderately water-soluble

may be directly related to the hydrophilic/hydrophobic nature of the particulate. In the preferred embodiment, the hydrophilicity of poly(styrene divinylbenzene) particulate increases as more SO_3^- substitution occurs but the effect on capacity factor (k') is surprising because sulfonation above about 0.6 milli-equivalent/gram results in a decrease in the capacity factor, (k'). Optimization of capacity factor (k') in the prior art involved choosing among various functionalized particulate. This invention teaches modification of the adsorptive character of a given particulate by controlled functionalization of the particulate with appropriate levels of certain functional groups.

Any of the particulate material may have a spherical shape, a regular shape or an irregular shape. Particulate material which has been found useful in the invention has an average size within the range of 0.1 to about 150 micrometers, preferably in the range of 0.1 to 100 micrometers, more preferably 1 to 100 micrometers, and most preferably 5 to 20 micrometers. It has been found advantageous in some instances to employ particulate materials in two or more particle size ranges falling within the broad range. As an example, particles of the present invention having an average size in the range of 0.1-30 micrometers having solid phase extraction capability may be employed in combination with particles having an average size in the range 1 to 150 micrometers acting as a property modifier. Larger particulate (e.g., 40 to 150 micrometers, even up to 4 mm or higher for industrial applications) are particularly desirable for packed columns and some nonwoven webs.

As noted above, more than one type of functionalized poly(styrene divinylbenzene) particulate

can be useful in columns and membranes of the present invention. The functionalized particles can be pre-mixed in any proportion; the total functionalized SPE particles of this invention can be present in the range
5 of more than 20 up to 100 weight percent of the total particles, preferably 35 to 100 weight percent, more preferably 50 to 100 weight percent organic polymeric particles, most preferably 90 to 100 weight percent derivatized organic polymeric particles of this
10 invention, and 0 to 80 weight percent of total particulate of any other SPE particles, preferably 0 to 65 weight percent, and more preferably 0 to 50 weight percent, and most preferably 0 to 10 weight percent of other SPE particles. Other SPE particles include
15 porous organic-coated or uncoated particles, and porous organic polymeric particles which can be functionalized or unfunctionalized.

In another aspect, the present invention provides an improved SPE composite structure and method
20 therefor, the composite structure preferably being a uniformly porous composite sheet comprising sorptive particles of the invention distributed uniformly throughout a fibrous matrix formed of nonwoven fibers. In such a structure almost all of the particles are
25 separate one from another and are entrapped in a matrix of fibers that restrains the particle. The preferred sheet of the invention has a thickness in the range of 125 to 10,000 micrometers. The ratio of total particles to fibrous matrix is in the range of 40:1 to
30 1:4, preferably 19:1 to 4:1, by weight.

In particle-loaded composite articles of the invention, property modifiers and adjuvants may be advantageously added to the primary particulate material in the fibrous medium to provide further
35 improvement in or modification of properties. For

example, modifier particulate can include inactive materials such as low surface area glass beads to act as property modifiers and processing aids. Coloring or fluorescing particulate can be added at low levels (up
5 to 10 weight percent of particulate) to aid in visualizing sample components to be separated. Chemically active particulate adjuvants which indicate chemical activity or acidity of the sample components can be useful for diagnostic purposes.

10 When the present invention particles are incorporated into particle-loaded fibrous articles, which preferably are microfibrous articles, the articles comprise in the range of 20 to 80 volume percent fibers and particulate, preferably 40 to 60
15 volume percent fibers and particulate, and 80 to 20 volume percent air, preferably 60 to 40 volume percent air.

Fibrous matrices useful for incorporation of the particulate of the invention include nonwoven webs,
20 such as nonwoven polymeric webs including polytetrafluoroethylene (PTFE), polyolefins such as polyethylene or polypropylene, polyaramid (e.g., Kevlar™, Dupont), polyamides such as nylon 6 and nylon 66, polyurethanes, polyesters such as polyethylene
25 terephthalate, polyacrylonitrile (Cyanamid, Wayne, NJ); other nonwoven webs include glass fiber webs and ceramic fiber webs.

PTFE provides a particularly useful fibrillated matrix for the present invention derivatized
30 particulates. The composite article can be prepared, for example, by the methods disclosed in any of U.S. Patent Nos. 4,810,381, 4,985,296, 5,071,610, 5,279,743, and 4,985,296.

Other webs useful for incorporating particles of
35 the present invention include nonwoven macro- and

microfibrous webs such as melt-blown webs, spunbonded or air-laid webs, blown fibrous webs. Making and using such webs is disclosed in U.S. Patent No. 5,328,758. Pressing or fusing of the webs is generally not
5 required in the articles of the present invention. Also useful can be glass fiber or ceramic fiber webs.

The particulate-containing fibrous webs of the invention can be useful in a first mode wherein the composite article of the invention is used for
10 preconcentration and isolation of certain materials for further analysis by, for example, high resolution column chromatography. In this mode, which is well known in the art and commonly called solid phase extraction, solvent and sample flow are introduced at
15 an angle of about 90 degrees to the surface of the sheet. This is a conventional configuration and the separation path length is equal to the thickness of the sheet. The path length can be increased by stacking additional layers (media) which may be the same or of
20 different composition but the individual layers need not be intimately bound together. This mode is effective for one step or multi-step adsorption-desorption separations. This mode is effective using sorptive ion exchange particulate in the normal or
25 reverse phase modes. The article strongly adsorbs the analyte of interest onto the active particulate in the composite and undesirable components are washed out with a first eluant. Conversely, undesirable components can be strongly bound and the analyte can be
30 washed out with the first eluant. A more effective eluting solvent is then used to displace the desired component from the particulate allowing it to be recovered in a more concentrated and unified form.

The composite extraction articles of the invention
35 can be of a variety of sizes and shapes. Preferably

the articles can be sheet-like materials which, for example, can be in disk or strip form.

This invention discloses a solid phase extraction (SPE) disk/sheet composite material and a method which is effective, for example, in isolating polar, semi-polar, and nonpolar organic contaminants from fluids (gases and liquids). The article can be used as a single self-supporting sheet, or a combination of sheets to form a stack, or as a composite film adhered to supports, such as glass, paper, metals, or polymers. The article is preferred for polar and semi-polar analytes. In particular, residues of explosives, phenolic compounds, and organic acids are common contaminants of solids, air, and water, and can be efficiently removed, concentrated, or isolated using the teachings of the present invention. The isolations can be performed on an analytical scale or in large scale applications.

Analytes which are nonpolar, i.e., minimal dipole moment, are hydrophobic and usually exhibit high capacity factor (k') levels with hydrophobic sorptive particles such as C_{18} bonded silica and neutral macroporous resins such as poly(styrene divinylbenzene). Using the functionalized particles of the present invention, these non-polar analytes are not expected to exhibit substantial increases in (k') values compared to those (k') increases found for polar and semipolar analytes. Some elevation of capacity factor (k') can occur due to increased surface area available from access to wetted internal pores.

Representative polar and semi-polar compounds (analytes) which can be sorbed by the functionalized particles of the present invention include explosives such as 1,3,5,7-tetranitro-1,3,5,7-tetraazacyclooctane (HMX), explosive impurities such as dinitrotoluene, and

phenolic compounds such as phenol, 2-chlorophenol, 4-chlorophenol, o- or p-cresol, 2- or 4-nitrophenol, 4,6-dinitro-o-cresol, 2,4-dinitrophenol, 2,4-dimethylphenol, 4-chloro-3-methylphenol, 2-methyl-4,6-dinitrophenol, pentachlorophenol, 2,4-dichlorophenol, 2,4,5-trichlorophenol, and 2,4,6-trichlorophenol, and catechol, which are pollutants in water and which are of environmental concern. Representative pesticides, generally considered semi-polar compounds, which can be recovered from aqueous liquids include atrazine, alachlor, and diazinon. Representative drugs, generally considered semi-polar compounds, include d-amphetamine, methamphetamine, salicylate, ibuprofen, butalbital, acetaminophen, amobarbital, pentobarbital, secobarbital, glutethimide, phencyclidine (PCP), phenobarbital, naproxyn, methadone, methaqualone, propoxyphene, cocaine, imipramine, desipramine, phenytoin, codeine, morphine, and flurazepam.

Neutral analytes such as ethyl pyruvate and butanedione exhibit a maximum capacity factor within the concentration range of the invention. These compounds are commonly extracted from water using liquid/liquid extractions (LLE), described in EPA Method 608, 625, etc. It is highly desirable to replace liquid-liquid extraction (LLE) methods with solid phase extraction (SPE) materials and methodology to reduce or eliminate extraction solvent usage, extraction time, and environmental hazards. This aspect of the invention discloses using a hybrid of column particle and membrane technologies to provide a means of overcoming the deficiencies of conventional methods with substantial savings in time and cost.

It has been found advantageous where combinations of contaminants are to be extracted to use a stack of disks (e.g., 2 to 5 or more) with one or more types of

particulate chosen, each having optimum extraction or reaction efficiency for individual contaminants. Choice of elution solvents depends on contaminants and extraction particulate.

5 This invention is useful in the extraction of inorganic and organic substances from liquids and gases in a flow-through or filtration mode. The invention can be used on an analytical scale, as in the testing of water samples for environmental pollutants. This
10 invention can also be used on a larger scale as in the remedial removal of contaminants or analytes from liquid or gas sources.

After use, the article can be recycled by simply eluting the sorbed pollutants from the article using a
15 liquid capable of removing the sorbed materials from the sorbent. Heat or supercritical fluid displacement or elution of the sorbed analyte can also be used.

Particles which can be loaded in a packed column and composite articles of the invention have utility in
20 a wide variety of separations wherein the choice of the particulate material is useful for size controlled filtration or steric exclusion, for simple one step or multistep sorption-desorption separations of specific components, for applications where sorptive particulate
25 perform chemical or biochemical separations, for ion-exchange conversions of cations and anions, for purification of materials, and for chromatographic separations and analyses in both passive and forced flow modes, for hydrophobic reverse phase and normal
30 phase chromatography, all being processes which are known to those skilled in the art.

Objects and advantages of this invention are further illustrated by the following examples, but the particular materials and amounts thereof recited in
35 these examples, as well as other conditions and

details, should not be construed to unduly limit this invention.

EXAMPLES

5

Example 1 -- Chemical modification of poly(styrene divinylbenzene)

A first procedure utilized 2 gram portions of 8 micrometer poly(styrene divinylbenzene) (SDVB) resin particulate from Sarasep, Santa Clara, CA. Eight resin samples were each mixed with 2 milliliters of glacial acetic acid to form a slurry. Concentrated sulfuric acid was added sequentially in fifty milliliter portions to each of these slurries and allowed to react at different temperatures and for different times. The reactions were then quenched by dilution of the sulfuric acid in the mixture with water and the resin particles were separated by filtration. After washing with water and drying, the degree of sulfonation of each sample was determined by titration with a standard solution of sodium hydroxide to determine ion exchange capacity in milliequivalents per gram. Reaction times, temperatures, and exchange capacity in milliequivalents per gram are listed for these samples in Table 1.

25

TABLE 1
Sulfonation levels of poly(styrene divinylbenzene)

	Sample No.	Reaction Time (minutes)	Temperature (degrees C)	Ion Exchange Capacity (meq./gm)
5	1 (comparative a)	--	--	0.0
10	2	0.5	0	0.1
	3	2	0	0.4
	4	4	0	0.6
	5	10	25	1.0
	6	20	25	1.2
15	7	90	25	1.5
	8	90	50	2.1
	9 (comparative b)	90	85	2.7

20

Sample 1 (comparative a) was unfunctionalized poly(styrene divinylbenzene) starting material and Sample 9 (comparative b) represented a typical strong cation exchange resin which had been heavily sulfonated (ion exchange capacity outside the present invention concentration range).

A second procedure for chemically modifying poly(styrene divinylbenzene) comprised mixing 5 ml of glacial acetic acid and 5 ml of concentrated H_2SO_4 with a sample of the base resin. A 60-minute reaction at room temperature produced a dark orange resin, but it was not wettable. Finally a reaction time of 5-10 minutes was used with heating (100-150°C). These resins were dark brown and wettable by aqueous solutions. The final resin with a capacity of 0.7 meq SO_3^- /g was made by the following conditions:

Two g. of macroporous poly(styrene divinylbenzene) resin (Sarasep, Inc.) were dried with gentle heat (100°C for 5-10 minutes). Glacial acetic acid (5 mL) was added and the mixture was placed in an oil bath at 150°C. Concentrated H₂SO₄ (5 mL) was added and the mixture was vigorously stirred with a cross-shaped magnetic bar for 5 minutes. The reaction was quenched by pouring the mixture into 100 mL of cool H₂O. The aqueous mixture was filtered and rinsed with successive 100 mL portions of deionized water, acetone, and methanol. The functionalized polymeric resin was then dried at approximately 100°C for several hours.

The resin was pre-wetted with methanol and then solid phase extraction of several phenols was performed with this resin (50 mg of resin particles packed in a small SPE column (20 mm x 2.1 mm ID). Each phenol was present in 15 mL of H₂O. After SPE was performed, each phenol was eluted with 1 mL of methanol. Recoveries (average of three trials) are listed below in Table 2.

20

TABLE 2 SPE of Phenols Using Sulfonated Resin	
Compound	Percent Recovery
phenol	95%
2-chlorophenol	96
4-chlorophenol	93
p-cresol	92
2,3-dichlorophenol	82

30

Example 2 -- Capacity factor (k') vs ion exchange capacity

Samples 1 through 9 listed in Table 1 were packed into a column to evaluate the effect of various levels

of sulfonation of the poly(styrene divinylbenzene) on sorptive capacity. A series of relatively hydrophilic compounds including phenol, catechol, ethyl pyruvate (a neutral ester), and 2,3-butanedione (a neutral ketone) were then passed through the column without methanol pre-wetting to determine capacity factors (k'). Data obtained is listed in Table 3.

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TABLE 3 Analyte Capacity Factors with Unwetted Particles					
Sample	Capacity*	Capacity Factor (k')			
		Phenol	Catechol	Ethyl pyruvate	Butane-dione
1	0.0 (compara- tive)	21	1	0	1
2	0.1	40	1	0	0
3	0.4	272	34	40	3
4	0.6	436	60	60	12
5	1.0	315	59	54	8
6	1.2	290	56	38	7
7	1.5	183	38	26	6
8	2.1	80	16	9	3
9	2.7 (compara- tive)	47	10	5	2

* SO_3^- ion exchange capacity in milli-equivalents/gram from Table 1.

Example 3 -- Capacity factor (k') vs ion exchange capacity

Examination of data in Table 3 shows that the capacity factor (k') in each case reached a maximum value when the ion exchange capacity was about 0.6 milliequivalents per gram. A second trial was performed using the particulate wetting procedure described by

Hagen et al., Analytica Chimica Acta, 236 (1990) 157-164, and the results are shown in Table 4.

5

10

15

TABLE 4 Analyte Capacity Factors With Wetted* Particles					
Sample	Ion Exchange Capacity**	Capacity Factor (k')			
		Phenol	Catechol	Ethyl pyruvate	Butane- dione
1	0.0 (compara- tive)	49	10	0	1
2	0.1	124	32	4	2
3	0.4	350	45	49	4
4	0.6	457	90	79	14
5	1.0	381	70	55	8
6	1.2	324	78	57	7
7	1.5	209	45	34	6
8	2.1	127	25	16	4
9	2.7	55	12	6	2

20 * particulate wetted with methanol

** SO₃⁻ ion exchange capacity in milliequivalents/gram

Examination of data in Tables 3 and 4 show that the capacity factor (k') for the ester, ketone and phenolics in each case reached a maximum value when the ion exchange capacity was about 0.6 milli-equivalents per gram of particulate.

Figure 1 illustrates graphically the optimization of the capacity factor (k') by controlling the degree of sulfonation of the particulate.

It is important to note that the unfunctionalized particulate gives a low value for the capacity factor (k'). The poly(styrene divinylbenzene) particulate that was more highly sulfonated and is typical of a cation exchange resin of prior art also gave a low value for

the capacity factor (k'). The maximum capacity factor (k') value occurred at about 0.6 milliequivalents/gram for the sulfonated particle but can vary for other functional groups such as the acetyl or hydroxyl groups which increase wettability.

More particularly, in the Drawing, Fig. 1 shows four plots from data of Table 6 of phenol capacity factor (k') vs. ion exchange capacity of poly(styrene divinylbenzene) resins. More specifically, in each run the particles were 5-8 micrometer average diameter and were packed in a column 20 mm x 2.1 mm ID. Plot A shows data of a run using methanol wetted sulfonated poly(styrene divinylbenzene) particles (sample 4 of Table 1); plot B shows data of a run using non-wetted sulfonated poly(styrene divinylbenzene) particles (sample 4 of Table 1); plot C shows data of a run using a mixture (sample 10b of Table 6) of sulfonated poly(styrene divinylbenzene) particles (sample 9 of Table 1) and unfunctionalized poly(styrene divinylbenzene) particles (sample 1, Table 1), the particles having been wetted with methanol before the run; plot D shows data of a run using a mixture of non-wetted sulfonated poly(styrene divinylbenzene) particles (sample 9 of Table 1) and unfunctionalized poly(styrene divinylbenzene) particles (sample 1, Table 1). Plots A, B, C, and D show that there is a maximum capacity factor (k') achieved when the ion exchange capacity of the derivatized poly(styrene divinylbenzene) is in the range of 0.1 to 2.5 milliequivalents, preferably 0.15 to 2.0 milliequivalents per gram, and more preferably 0.2 to 1.1 milliequivalents. For wetted and non-wetted particles, there is a maximum capacity for phenol achieved when the ion exchange capacity of the functionalized poly(styrene divinylbenzene) is in the

range of 0.1 to 2.5 milliequivalents per gram of functionalized poly(styrene divinylbenzene), preferably 1.5 to 2.0 and most preferably 0.2 to 1.1 milliequivalents. Wetted particles provide optimal capacity factor (k') of functionalized poly(styrene divinylbenzene) particles. As shown by plots C and D, a mixture of functionalized and non-functionalized particles provided very little increased capacity factor (k') with increase in ion exchange capacity, although the wetted particles showed some benefit in capacity factor (k') compared to a mixture of non-wetted particles.

Example 4 -- PTFE composite membranes comprising 80% of sample 4 sulfonated poly(styrene divinylbenzene) (0.6 meq/gm ion exchange capacity) and 20% by weight PTFE were evaluated for their ability to extract a series of phenolic compounds listed in Table 5 below. The recoveries obtained were compared to those obtained for PTFE composite membranes comprising 20 weight percent PTFE and 80 weight percent AmberChrome 71 resin, which was disclosed in U.S. Patent No. 5,279,742, as a desirable sorptive particle. One hundred parts per billion by weight of each phenol were prepared in a 500 milliliter volume of deionized water. The pH was adjusted to 2.0 with HCl and 10% by weight NaCl was added to help salt out the soluble phenols from the aqueous phase to the sorptive solid phase. This procedure is well known in the art. Lowering the pH assures that the phenols are protonated for better transfer to the hydrophobic SPE media.

The water sample containing the phenolic analytes was pulled through the SPE membrane (47 mm diameter) using a standard filtration apparatus (Millipore Corp., Bedford, MA) with water aspirator vacuum of 66 cm (26

inches) of Hg. After the extraction step, the phenolic analytes were eluted from the membrane with 3 successive 3 mL aliquots of tetrahydrofuran (THF). The 3 aliquots were combined and THF was added to give a final volume of 10 milliliters for analysis by liquid chromatography. The analytical results listed in Table 5 are an average of 4 determinations for the sulfonated poly(styrene divinylbenzene) and 3 determinations for the AmberChrom 71.

10

Table 5 Recovery Data for the SPE of Phenols		
Compound	Percent Recovery	
	Sulfonated poly (styrene divinyl- benzene) (0.6 meq/gm)	AmberChrom 71
phenol	79.0	9.6
4-nitrophenol	94.7	27.2
2,4-dinitrophenol	85.4	26.9
2-nitrophenol	65.8	16.7
2,4-dimethylphenol	72.4	20.7
4-chloro-3-methylphenol	85.1	28.7
2-methyl-4,6-dinitrophenol	79.5	33.6
2,4,6-trichlorophenol	75.9	30.0
pentachlorophenol	96.1	37.2

30

The data show the recoveries obtained for the sulfonated poly(styrene divinylbenzene) were considered very good for these phenols compared to those obtainable using a conventional sorptive particulate, AmberChrom 71.

35

Example 5: Capacity factor (k') for phenol versus degree of sulfonation of poly(styrene divinylbenzene) sorbent

Data in Table 6 (which contains data of Tables 3 and 4, columns 1-3 for samples 1-9) show that an optimum capacity factor (k') can be achieved by controlled functionalization of the poly(styrene divinylbenzene) polymer particles. In additional trials, simple mixtures of the un-sulfonated (neutral) particles and heavily sulfonated particles (strong cation exchange) as illustrated by samples 10a, 10b, and 10c did not achieve optimization of the capacity factor (k') as shown by samples 1 - 9.

15	Table 6 Capacity factor (k') for phenol vs. degree of sulfonation of poly(styrene divinylbenzene) sorbent			
20	Sample number	Ion Exchange Capacity (meq. SO_3^- /gm)	CH_3OH Wetted (k')	Non-wetted (k')
	1(a)	0.0	49	21
25	2	0.1	124	40
	3	0.4	350	272
	4	0.6	457	436
	5	1.0	381	315
	6	1.2	324	290
30	7	1.5	209	183
	8	2.1	127	80
	9(a)	2.7	55	47
	10a*(a)	0.0	50	21
	10b**	0.6	56	33
35	10c*(a)	2.7	53	47

- (a) comparative
* second trial of samples 1 and 9 respectively to
compare (k') of mixtures
** mixture of portions of samples 10a and 10c give
5 sample 10b with a net ion exchange capacity of 0.6
meq SO_3^-/gm

Example 6:

A. Samples of macroporous poly(styrene
10 divinylbenzene) resins with various concentrations of
carboxylic acid functionality (a weak cation exchange
group) were prepared as described by R. Kunin in "Ion
Exchange Resins", 2nd edition, Wiley:New York, (1958)
p. 87, and by Meitzner et al. in U.S. Patent No.
15 4,256,840 wherein the ion exchange capacities were
varied by changing the ratio of methacrylic acid,
divinylbenzene and styrene starting monomers. These
samples with ion exchange capacities ranging from 0 for
non-carboxylated base poly(styrene divinylbenzene), to
20 0.3, 2.9, and 5.8 milliequivalents per gram for
carboxylated resins, were incorporated into 0.5 mm
thick PTFE sheet material comprising 20 percent PTFE
and 80 percent by weight of each resin particulate
using a process described in U.S. Patent No. 5,147,539.
25 Forty seven millimeter diameter disks were cut from
these sheet materials and the particle loaded disks
comprising particles with varying ion exchange
capacities were individually tested for SPE efficiency
using the phenolic analytes listed in Table 5.
30 In these trials, 500 milliliter test samples
containing a mixture of 100 parts per billion (100 μg
per liter) of each phenolic analyte in distilled water
were adjusted to a pH of 2 with hydrochloric acid.
(Acidification is often used to suppress ionization and
35 keep the phenolic analyte in the protonated form to
enhance extractability by reverse phase particulate.)
Samples were pulled through the disks mounted in a

standard Millipore™ filtration apparatus using a vacuum of 66 cm (26 inches) Hg. Phenolic analytes adsorbed from these water samples by the resin loaded disks were subsequently desorbed i.e., eluted from the disks using 5 2 sequential 10 milliliter portions of tetrahydrofuran (THF) which were then combined and brought to 25 milliliter analytical volumes with THF. These eluant solutions were analyzed by liquid chromatography to measure the phenolic analyte content to determine the 10 percent recovery obtained by the SPE process. The data is shown in Table 7A, below.

Table 7A
Percent Recovery of Phenols vs Ion Exchange Capacity of Carboxylated SDB Copolymer Resin

Exchange Capacity (meq/gm)	phenol	4-nitro phenol	2,4-dinitro phenol	2-nitro phenol	2,4-dimethyl phenol	4-chloro, 3-methyl phenol	2,4-dichloro phenol	2,4,6-trichloro phenol	pentachloro phenol
0*	7.0	37.0	105.4†	104.1†	108.3†	85.6	91.9	102.1†	93.2
0.3	16.4	94.1	99.7†	98.0	104.9†	83.2	89.7	96.8	91.8
2.9	12.5	60.5	89.0	90.1	92.0	73.9	83.8	91.1	94.8
5.8	10.1	45.6	78.6	93.4	87.2	80.2	91.9	102.1†	93.2
Average % RSD**	13.4	3.0	2.6	2.7	4.0	5.4	4.3	4.6	3.6

* represents comparative sample of unfunctionalized poly(styrene divinylbenzene)

** relative standard deviation

† recoveries above 100% represent experimental scatter

Data in Table 7A indicate that good recoveries were found for the less polar phenolics tested (i.e., 2-nitrophenol, 2,4-dimethyl phenol, 4-chloro-3-methyl phenol, 2,4,6-trichlorophenol, and pentachlorophenol) with little dependence on the level of carboxyl groups present on the poly(styrene divinylbenzene)sorbent. Better recoveries were obtained for the more polar phenolic analytes (phenol and 4-nitrophenol). In particular, phenol and 4-nitrophenol exhibited a definite maximum percent recovery with the resin sample which had 0.3 milli-equivalents per gram ion exchange capacity level of carboxylate group. Recovery levels for 4-nitrophenol subsequently decreased when higher levels of carboxyl groups were present. Recoveries of the 2-nitrophenol isomer were consistently high regardless of the level of carboxylate group substitution. This is not unexpected since the close proximity of the nitro and phenol groups favors intramolecular hydrogen bonding and results in decreasing water solubility. The 2,4-dinitrophenol analyte recoveries were higher than those found for 4-nitrophenol but also decreased with increasing levels of carboxylate substitution of the sorptive resin particulate.

B. In another set of trials, a series of partially carboxylated copolymer resin particulates were prepared via the method as described by Kunin (see Example 6A) using various levels of methacrylic acid monomer. These resin particles were incorporated into PTFE membranes comprising 80 weight percent particles and 20 weight percent PTFE as described above. The resulting composite articles were evaluated for sorptive properties using polar probe compound analytes; phenol, 4-nitrophenol, and neutral probe analytes: dimethyl phthalate (DMP), diethyl phthalate

(DEP), dibutyl phthalate (DBP), dioctyl phthalate (DOP), and o-methyl anisole (OMA) (an ether).

Experimental procedure was the same as for Table 7A, except that the analytes were present at 5 parts per 5 million (5 mg per liter) and methanol was present at two percent by volume due to sample preparation procedures. The data of Table 7B show the percent recoveries obtained. Maxima occurred at the level of 0.3 milliequivalent carboxylate functionality per gram 10 of copolymer resin for phenol and 4-nitrophenol. The phenol and 4-nitrophenol analytes are polar and showed low capacity factors (k') which gave lower percent recovery levels using the poly(styrene divinylbenzene) copolymer resin based particles. The phthalate esters 15 and o-methyl anisole are neutral analytes and had high capacity factors (k') as shown by the near 100 percent recovery levels, and no effect on recovery levels was observed with different levels of carboxylate functionality.

20

TABLE 7B									
Percent Recovery vs. Ion Exchange Capacity of Carboxylated Poly(styrene divinylbenzene) Copolymer Resin									
	Exchange Capacity meq/gm	phenol	4-nitrophenol	DMP	DEP	DBP	DOP	OMA	
1	0.0	3.4	13.2	99.6	99.3	98.4	98.6	96.8	
2	0.3	4.8	19.8	100.6	99.8	99.1	98.1	95.9	
3	0.6	3.5	14.3	100.0	99.2	98.7	98.2	96.2	
4	0.9	3.3	14.4	100.0	99.6	98.9	98.3	96.6	
5	1.5	4.1	16.3	99.3	99.3	98.0	97.4	95.8	

5

10

It is recognized in the art that analyte capacity factor (k') values are directly proportional to analyte recovery levels in SPE processes. Data of Tables 7A and 7B show that controlling the level of carboxyl functionality on poly(styrene divinylbenzene) copolymer resin can be used to maximize extractability of certain analytes.

Example 7: Comprehensive Serum and Urine Drug Screens

10 Disks comprising 20 percent PTFE and 80 percent sample number 4 from Table 3, Example 2 (poly(styrene divinylbenzene) particulate functionalized with sulfonate functional group at an ion exchange capacity of 0.6 meq/gm) were tested in a comprehensive drug
15 screening procedure. The results were compared with data obtained using disks comprising 20 percent PTFE and 80 percent Clean Screen™ (CS) particulate from United Chemical Technology, Bristol, PA (commercially available silica based particles coated with a mixed
20 phase comprising an octyl reverse phase group and a strong cation exchange functionality). Results were also compared with data obtained using TOXI-TUBES for acidic and basic drug extractions from urine, commercially available from Toxi-Lab, Inc., Irvine, CA.

25

Materials and Methods

Drug Standards

Stock standard solution used was 100 µg/mL of each of the following drugs in methanol:

30	d-amphetamine	naproxyn
	methamphetamine	methadone
	salicylate	methaqualone
	ibuprofen	propoxyphene
	butalbital	cocaine
35	acetaminophen	imipramine

	amobarbital	desipramine
	pentobarbital	phenytoin
	secobarbital	codeine
	glutethimide	morphine
5	phencyclidine (PCP)	flurazepam
	phenobarbital	

Internal standard solution used was 0.5 mg/mL cyheptamide in methanol.

10 Extraction Procedure -- Extraction Disk Cartridges (3M Co., St. Paul, MN), (Columns B and C in Table 8)

1. Samples were prepared as follows:

Urines: Sequentially were added 3 mL distilled water, 2 mL 0.1 M phosphate buffer (pH =
15 6.0), and 10 μ L of internal standard solution to 2 mL of urine (spiked with an appropriate amount of drug standard). Samples were thoroughly shaken.

Serums: Sequentially were added 4 mL distilled water, 2 mL 0.1 M phosphate buffer (pH =
20 6.0), and 10 μ L of internal standard solution to 1 mL of serum (spiked with an appropriate amount of drug standard). Samples were thoroughly shaken.

2. The extraction disk cartridge was conditioned with sequential additions of one 3-mL volume of
25 methanol, one 3-mL volume of distilled water, and one 1-mL volume of 0.1M phosphate buffer (pH = 6.0). Each addition was aspirated but the disk was not allowed to dry.

3. Sample was applied and aspirated at full
30 vacuum.

4. Disk cartridge was washed with one 3-mL volume of distilled water followed by one 1-mL volume of 1.0M acetic acid. Disk cartridge was dried at full vacuum for 5 minutes, then washed with one 2-mL volume
35 of hexane.

5. Elution of acidic and neutral drugs was accomplished using one 3-mL volume of hexane/ethyl acetate (50/50); the eluate was collected at less than 5 mL/minute, then transferred into a conical bottom dry 5 down tube.

6. The disk cartridge was washed with one 3-mL volume of methanol and dried at full vacuum for 5 minutes.

7. Basic drugs were eluted with one 2-mL volume 10 of elution solvent (24 mL methylene chloride, 6 mL isopropanol, and 0.9 mL ammonium hydroxide; made fresh daily). Eluate was transferred into the same tube as the previous eluate.

8. The eluate sample was concentrated by drying 15 under a gentle stream of compressed air without heating. When completely dry, 150 μ L of chloroform was added to the residue and the sample was thoroughly mixed.

9. Sample was analyzed by injecting 1 μ L of 20 chloroform solution containing the analytes into a chromatograph.

Extraction Procedure -- Liquid-Liquid Extraction for Urines (Columns D and E in Table 8)

25 1. Each extraction tube was prepared by adding 2 mL of urine (spiked with an appropriate amount of drug standard) and 10 μ L of internal standard solution (described above) to TOXI-TUBES (basic and acidic extractions).

30 2. Contents of each extraction tube was mixed by gentle inversion for a minimum of five minutes.

3. The tube was centrifuged at high speed for 5 minutes.

4. The organic layer was transferred to conical 35 bottom dry down tube.

5. The sample was concentrating drying the organic layer under a gentle stream of compressed air without heating. When completely dry, 150 μ L of chloroform was added to the residue and the tube was
5 shaken.

6. The sample was analyzed by injecting 1 μ L of chloroform containing the analytes into a chromatograph.

10 Extraction Procedure -- Liquid-Liquid Extraction for Serum (Column A in Table 8)

Stock Solution A:

Ammonium sulfate crystals were washed twice with methanol and dried at 100°C for several hours. A
15 supersaturated solution of the crystals was prepared in distilled water. Twenty mL of concentrated hydrochloric acid was then mixed with 250 mL of the supersaturated ammonium sulfate solution.

1. Each extraction tube was prepared by adding
20 0.4 mL of Stock Solution A with 10 μ L of internal standard (described above), to 1 mL of serum (spiked with an appropriate amount of drug standard). Nine mL of methylene chloride extraction solvent were then added.

25 2. The tube was shaken for 5 to 10 minutes.

3. The tube was centrifuged at high speed for 5 minutes.

4. The methylene chloride layer was transferred to a conical bottom dry down tube.

30 5. The sample was concentrated by evaporating the methylene chloride extraction solvent using a gentle stream of compressed air. When completely dry, 150 μ L of chloroform were added to the extracted residue and the sample was thoroughly mixed.

6. Analyze sample. One (1) μ L of chloroform containing the analytes was injected into a chromatograph for analysis.

Table 8 Detection of Drugs from Extracted Samples									
Drug	Serum Extractions				Urine Extractions				
	A(a) Liquid/ Liquid	B(a) Clean Screen™	C SCX/SDB	D Toxi-Tube™(a) Basic	E Toxi-Tube™(a) Acidic	B Clean Screen™	C SCX/SDB		
d-amphetamine	-	+	+	-	-	+	+		
methamphetamine	-	+	+	-	-	+	+		
ibuprofen	+	-	-	-	-	-	+		
butalbital	+	+	+	+	+	+	+		
amobarbital	+	+	+	+	+	+	+		
pentobarbital	+	+	+	+	+	+	+		
secobarbital	+	+	+	+	+	+	+		
glutethimide	+	+	+	+	+	+	+		
phencyclidine	+	+	+	+	+	+	+		
phenobarbital	+	-	+	+	+	-	+		
methadone	+	+	+	+	+	+	+		
methaqualone	+	+	+	+	+	+	+		
propoxyphene	+	+	+	+	+	+	+		
cocaine	+	+	+	+	-	+	+		
imipramine	+	+	+	+	+	+	+		
desipramine	-	+	-	+	-	-	+		
phenytoin	+	+	+	+	+	+	+		
codeine	+	+	+	+	-	+	+		
morphine	-	+	+	+	-	+	+		
flurazepam	+	+	+	+	-	+	+		

(a) comparative

- A Liquid/Liquid extraction -- conventional method
- B Clean Screen -- particle loaded web as a disk in a cartridge format
- 5 C SCX/SDB -- present invention particle loaded as web; a disk in a cartridge
- D Toxi-Tube Basic -- (comparative) liquid/liquid extraction
- E Toxi-Tube Acidic -- (comparative) liquid/liquid extraction
- 10

The data of Table 8 show that the present invention particle-loaded membranes were at least as good and in most instances better as a screening device
15 than conventional devices for establishing the presence of 20 commonly tested drugs.

Advantages of sulfonated poly(styrene divinylbenzene) particles in a membrane format for
20 comprehensive drug screening include eliminating the need for separate basic and acidic liquid/liquid extractions, and thus two injections for chromatographic analysis. The present invention membrane allows for one extraction (two elution
25 solvents are used and combined before dry down) and one injection for chromatographic analysis, which saves time.

The present invention membrane allows more drugs to be detected in the screening method when compared to
30 conventional liquid/liquid analyses [e.g., amphetamine, methamphetamine, morphine, codeine, cocaine (serum) and amphetamine, methamphetamine, ibuprofen, phencyclidine, phenobarbital (urine)].

The present invention membrane saves time and
35 money in this screening mode. Also, there is the

potential for automation using the present invention materials. Further, the present invention provides a lower detection limit for drugs.

5 Various modifications and alterations of this invention will become apparent to those skilled in the art without departing from the scope and spirit of this invention, and it should be understood that this invention is not to be unduly limited to the
10 illustrative embodiments set forth herein.

CLAIMS:

1. At least one functionalized macroporous poly(styrene divinylbenzene) particle wherein said
5 functionality consists essentially of at least one ionic functional group selected from the group consisting of SO_3H , COOH , $\text{N}^+(\text{R})_3$, wherein said R group independently is an alkyl group having 1 to 4 carbon atoms, and $\text{N}(\text{R}^1)_2$, wherein each R^1 independently is
10 hydrogen, alkyl or alkanol groups having 1 to 4 carbon atoms, said functional group being covalently bonded thereto, said functionalized particle having sorptive capability towards an organic analyte, said functional group being present in the range of 0.1 to 2.5
15 milliequivalents per gram of functionalized poly(styrene divinylbenzene), wherein said analyte exhibits a maximum in capacity factor (k') with respect to poly(styrene divinylbenzene) functionalized in the specified concentration range compared to (k') of the
20 same analyte for similarly functionalized poly(styrene divinylbenzene) outside the designated concentration range.

2. The particle according to claim 1 wherein
25 said functional group is a sulfonate (HSO_3) group.

3. The particle according to claim 1 wherein said functional group is a carboxylic acid (COOH) group.
30

4. The particle according to claim 1 wherein said functional group is at least one of a quaternary ammonium group $\text{N}^+(\text{R})_3$, wherein each R independently is selected from C_1 to C_4 alkenyl groups, and an aminated
35 group $\text{N}(\text{R}^1)_2$, wherein each R^1 is independently selected

from the group consisting of hydrogen, alkyl groups having 1 to 4 carbon atoms, and alkanol groups having 1 to 4 carbon atoms.

5 5. The particle according to any of claims 1 to 4 wherein said analyte is selected from the group consisting of phenolics, alcohols, ketones, ethers, and esters.

10 6. The particle according to any of claims 1 to 5 wherein said analyte is selected from the group consisting of explosive residues, pesticides, and drugs.

15 7. A particle packed column or bed comprising particles according to any of claims 1 to 6.

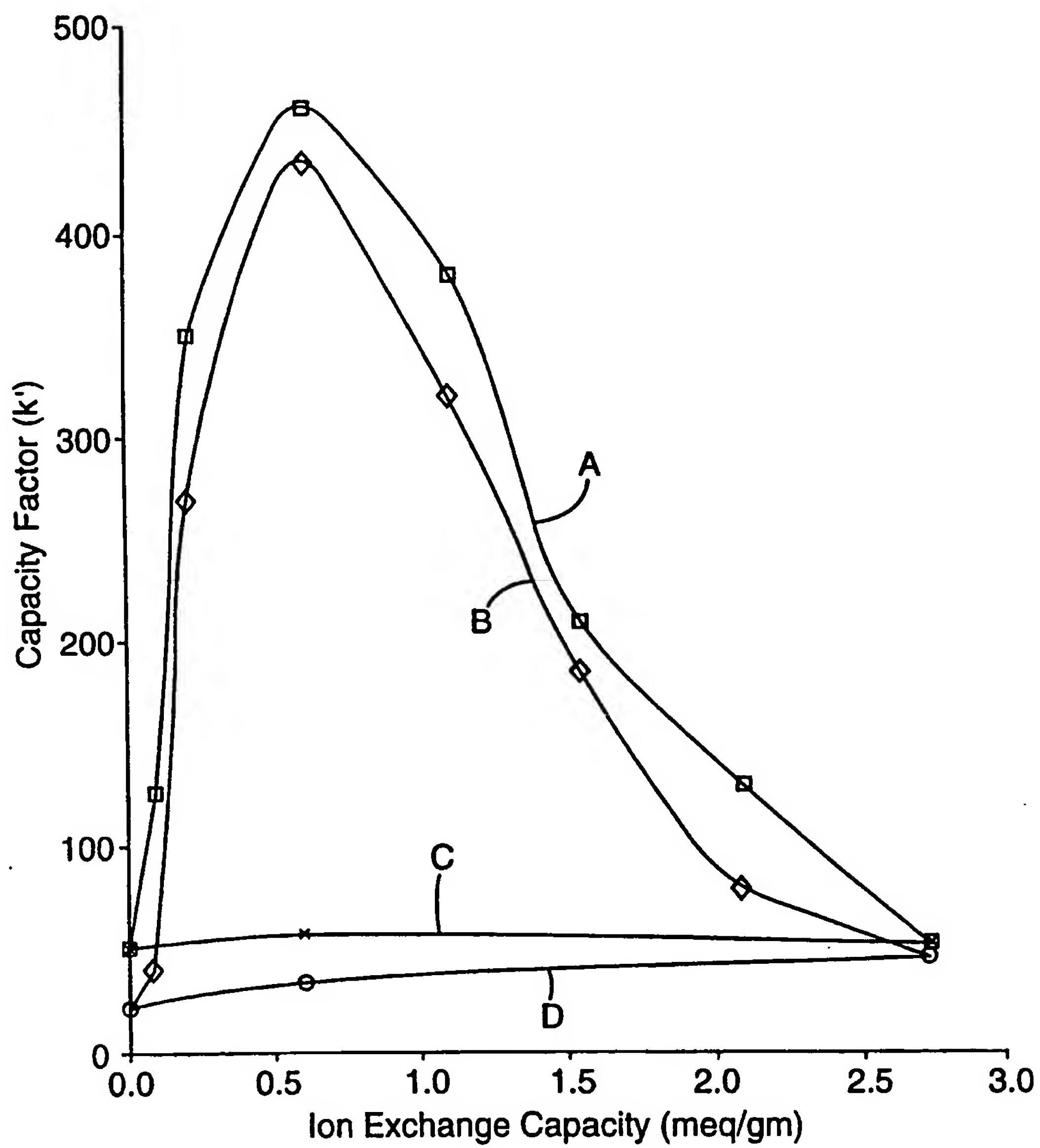
8. A method of optimizing the capacity factor (k') of an analyte using poly(styrene divinylbenzene) particles which are functionalized with at least one functional group, said method comprising the step:
providing a macroporous poly(styrene divinylbenzene) particles according to any of claims 1 to 6, said method further comprising the step of
25 contacting said functionalized particles comprising said functional group in said concentration range with said analyte for a time and at a temperature sufficient to bind said analyte to said particles, and said method further comprising the step of isolating said analyte
30 in a concentrated form by elution from said particles and regenerating said particles.

9. A solid phase extraction or reaction medium comprising
35 (a) a fibrous matrix, and

- (b) sorptive particles enmeshed in said matrix comprising
- (1) more than 20 and up to 100 weight percent of functionalized macroporous poly(styrene divinylbenzene) particles according to any of claim 1 to 6,
 - (2) less than 80 to 0 weight percent of porous, organic-coated or uncoated, inorganic particles,
- the ratio of particles to fibrous matrix being in the range of 40:1 to 1:4 by weight.

10. The medium according to claim 9 wherein said fibrous matrix is selected from the group consisting of polytetrafluoroethylene, polyolefins, polyaramids, polyamides, polyurethanes, cellulosics, glasses, and ceramics.

11. A method of isolating at least one analyte from a fluid comprising the step of:
passing a fluid containing the at least one analyte through at least one solid phase extraction medium according to claim 9, said method optionally further comprising the step of isolating said analyte in a concentrated form by elution from said particles and regenerating said particles.



INTERNATIONAL SEARCH REPORT

Inter nal Application No
PCT/US 95/03834

A. CLASSIFICATION OF SUBJECT MATTER

IPC 6 B01D15/00 B01J39/06 B01J41/06

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 B01D B01J

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

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A	see column 1, line 1-28 ---	
Y	US,A,3 489 699 (BATTARD) 13 January 1970 see page 2, line 40-70	1,5
A	see column 17-18; table 3 see column 10, line 10-28 see column 30-32; claims 1-9 ---	2-4,7,8
A	US,A,5 292 818 (OISHI) 8 March 1994 see column 9, line 53 - column 10, line 37 see column 11-12; example 1 ---	1
A	EP,A,0 556 879 (ROHM AND HAAS) 25 August 1993 see page 5, line 24 - page 6, line 28 ---	1-4
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Further documents are listed in the continuation of box C.



Patent family members are listed in annex.

* Special categories of cited documents :

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Date of the actual completion of the international search

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INTERNATIONAL SEARCH REPORT

International Application No
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Int: International Application No

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